

Field scale variability of soil structure and its impact on crop growth and nitrate leaching in the analysis of fertilizing scenarios

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ABSTRACT

Soil structure variability was inventoried on a field scale, and translated to basic input data for a solute transport and crop production simulation model. After validation of the model, it was used to simulate the spatially varying effect of slurry application and N-fertilizing scenarios by multiple point-simulations. Feasibility of scenarios was determined by comparing nitrate leaching concentrations with current and pursued threshold levels. Disjunctive kriging was used to estimate and map the probability that these threshold levels were exceeded.

Emphasis was given to the effect of soil-specific slurry application rates and N-fertilizer levels on leaching probabilities and crop yields. Soil-specific N-treatments increased field yields, because crop response to N, both in slurry and in fertilizer, was soil dependent. The leaching response to N-treatment was also soil dependent.

INTRODUCTION

Currently, legislation is being developed in the Netherlands to restrict inputs into the environment of polluting substances. Agriculture has been identified as a possible source of (e.g.) biocides, nitrates and ammonia. In order to make effective laws, possible effects of protective measures have to be evaluated by scenario analyses. In agricultural practice, management takes place on a field scale at farm level, and since the management can be influenced by legislation, scenario analyses should be carried out on the same field scale. Management scenarios can be analyzed by using simulation models. Input data should reflect field variability. This enables the evaluation of not only the average result of implementing a measure, but also its field scale variability. Knowledge about this variability allows the effect of an implemented measure to be expressed in terms of a probability distribution. Such a distribution can be used to estimate the probability that the effect of a measure is

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violating a statutory threshold value. Spatial variability of a variable can be translated into probability density functions by using the spatial prediction method disjunctive kriging.

This paper describes two scenario-analyses that were made to optimize the addition of organic manure and of inorganic fertilizer on a field scale with respect to nitrogen losses to atmosphere and groundwater. Special emphasis was given to the effect these additions would have on crop production. Both scenarios that were analyzed explicitly used soil structure variability to generate the dynamic soil physical characteristics water retention and hydraulic conductivity, and the static characteristics bulk density, texture and organic matter content. These characteristics were necessary to describe field scale variability of water flow and nitrogen fate by using a simulation model.

MATERIALS AND METHODS

Spatial variability of soil structure

The area under study is an agricultural field in the Wieringermeer polder in the northwestern part of the Netherlands. Soils were classified as fine-loamy, calcareous, mesic Typic Udifluvents (Soil Survey Staff, 1975) and show a highly variable soil structure. Soil structure variability was caused by the complex sedimentation history of the area, which was part of a mud-flat landscape of tidal channels separating shoals before it was reclaimed.

A problem encountered when the behaviour of these stratified soils is to be simulated, is how to discretize the soil profile. Obviously, the thin layers visible in a vertical section (Fig. 1) cannot be analyzed separately for the determination of soil physical characteristics, and cannot be recognized from auger-cores in a soil survey. However, vertical successions of these thin layers can be recognized by their over-all structure and can be analyzed. A study was dedicated to whether these generalised layers could serve as functional layers.

A functional layer is a layer that has functional hydrological properties significantly different from those of other functional layers, and has a low internal variability (Wösten et al., 1990; Finke et al., 1992). Functional properties used were (Wösten et al., 1986):

- (1) the *travel time* during a period of steady infiltration, and
- (2) the *maximal height above the water table* at which a defined upward flux can be maintained.

For the study area, Finke and Bosma (1993) concluded that soil profiles could successfully be generalized into a vertical sequence of three different functional layers, which were easily recognizable in a regular soil survey. The properties of different functional layers proved to be significantly different, and using the functional layers to generate input for a simulation model on a number of test plots resulted in accurate simulations.

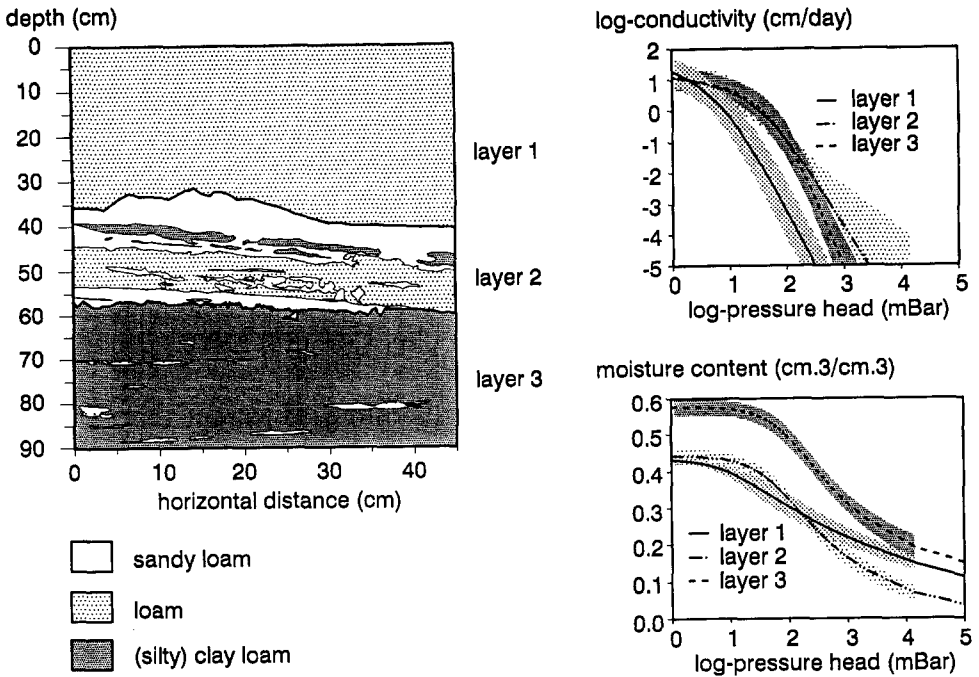


Fig. 1. Vertical section showing the thinly stratified soil profile and its generalization into three functional layers.

The problem of inventorying spatial variability of soil structure was thus reduced to mapping the thickness and depth of functional layers. A two-phase soil survey was made. In the first phase, a nested sampling scheme was followed (Webster, 1977) during which 93 profile descriptions were collected with the purpose to quantify variability at both short and longer ranges relative to the field scale. Based on variogram analysis and interpretation of aerial photographs it was decided to sample a triangular grid with a mesh of 16 m in the second phase of the soil survey (Finke, 1991). The resulting 402 profile descriptions that were collected, were used to produce a soil map (Fig. 2), and were translated into as many location-specific input files for computersimulations.

Model description

To perform the scenario analyses, an existing model (LEACHM, Hutson and Wagenet, 1991) was extended with a potato crop growth submodel. The model simulates water flow, nitrogen transformations and nitrogen transport and

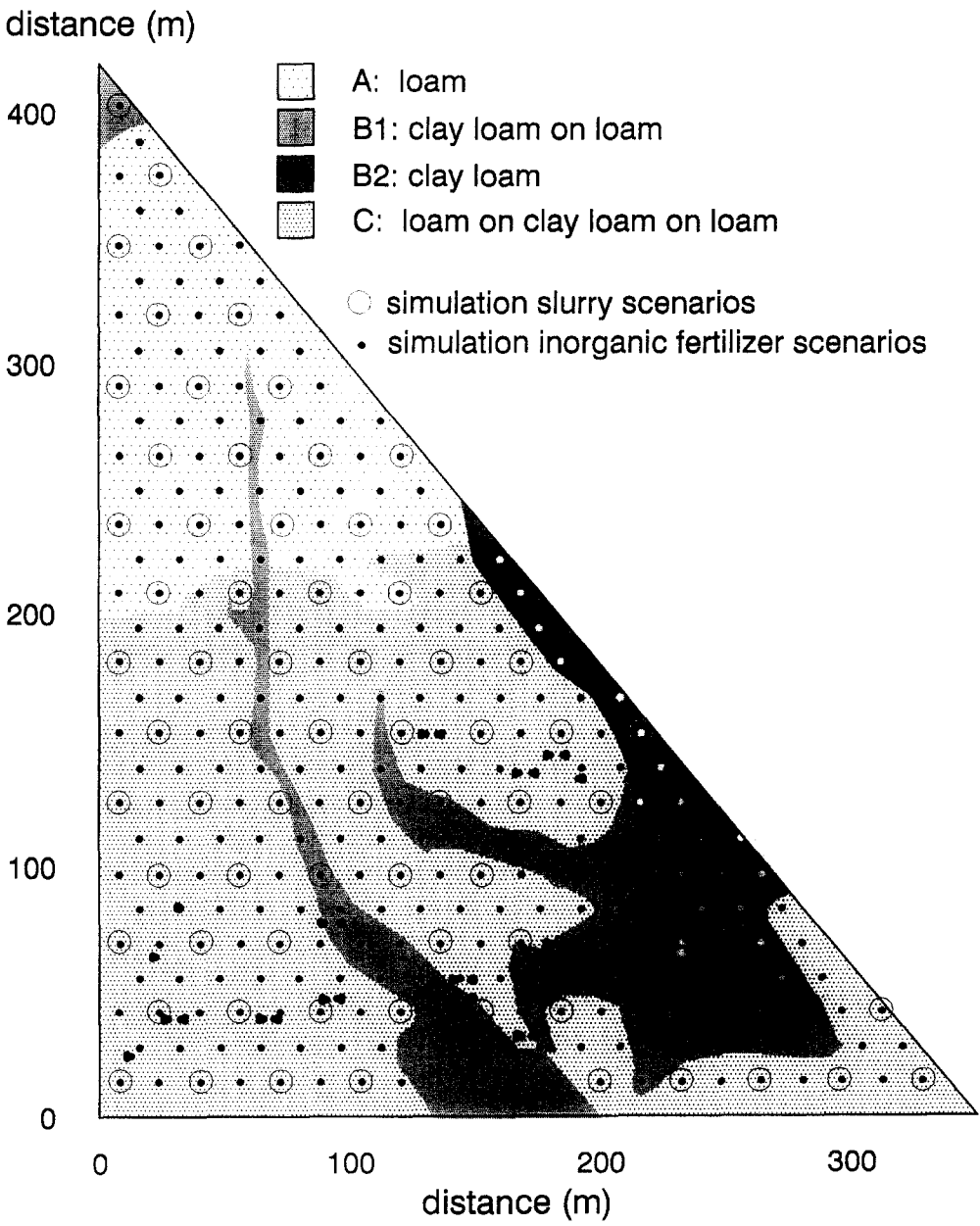


Fig. 2. Soil map and simulation locations used in the scenario analyses.

potato crop growth. The water flow is calculated using a finite-difference solution to the Richard's equation:

$$\frac{\partial \theta}{\partial t} = \left(\frac{\partial}{\partial z} \right) \left(K(\theta) \frac{\partial H}{\partial z} \right) - U(z, t) \quad (1)$$

where θ is the volumetric water content (m^3/m^3), t is the time (days), H is the hydraulic head ($100 \times \text{Pa}$), defined as $H = h - z$, where h is the soil matric potential and z is the depth in cm, K is the hydraulic conductivity (cm/day) and U is a sink term representing water lost by transpiration (cm). The daily potential transpiration was calculated by (Belmans et al., 1983):

$$T_p = ET_p \cdot [1 - \exp(-0.6I)] \quad (2)$$

where T_p is the potential transpiration (cm/day), ET_p is the potential evapotranspiration (cm/day) and I is the leaf area index (m^2/m^2). The functions between K , θ and h that are required, were described using the closed form equations by Van Genuchten (1980).

The performance of the water flow submodel, using functional layers to generate the hydraulic characteristics, was tested by comparison of measured and simulated matric potentials on five plots at three depths (Finke, 1992; Finke and Bosma, 1993).

Nitrogen cycling is described according to the concepts and equations of Johnsson et al. (1987). Three organic nitrogen pools, characterized as a quickly degrading manure and litter pool and a relatively stable humus pool, are distinguished in the model. Also a urea pool and mineral ammonia and nitrate pools are identified. Mineralization processes, volatilization, nitrification and denitrification are described by first-order rate constants, volatilization occurring only from the surface layer. Rate constants are adjusted for temperature and water content effects (Johnsson et al., 1987). Ammonium, nitrate and urea can be partially sorbed onto soil surfaces through a linear sorption isotherm. Chemical transport is simulated by a numerical solution to the convection-dispersion equation (Wagenet, 1983):

$$\frac{\partial(\theta c)}{\partial t} + \frac{\partial(\rho S)}{\partial t} = \frac{\partial}{\partial z} \left(\theta D(\theta, q) \frac{\partial c}{\partial z} - qc \right) - U(z, t) \pm \phi(z, t) \quad (3)$$

where c is the chemical concentration in the liquid phase (mg/dm^3), s is the chemical concentration in the sorbed phase (mg/kg dry soil), ρ is the soil bulk density (kg/dm^3), $D(\theta, q)$ is the effective dispersion coefficient (mm^2/day), q is the water flux density (mm/day), ϕ is a source/sink term ($\text{mg}/\text{dm}^3, \text{day}$) representing gains/losses through transformation and $U(z, t)$ is the plant uptake of nitrogen ($\text{mg}/\text{dm}^3, \text{day}$). The plant uptake of nitrogen is determined by the transpiration flux and concentrations in the compartments

$$S_n = \min \left[1, \frac{P_w - P_0}{P_M - P_0} \right] \quad (5)$$

where S_n is the stress factor for the current day, P_w is the actual %N in total dry matter, P_0 is the %N in total dry matter when growth ceases and P_M is the minimum %N in total dry matter to have the maximum growth rate.

The plant physiological age, characterized by the temperature-sum since the day of emergence, is used to partition the biomass increase to shoots, tubers and roots. Occurrence of stress due to limited nitrogen and/or water availability will cause the partitioning to be changed in favour of root growth and disfavour of shoot and tuber biomass growth. The leaf area index (LAI) is considered to be a linear function of the shoot biomass until a certain temperature-sum is reached, whereafter the LAI becomes a monotonically decreasing function of the temperature-sum and the shoot biomass according to:

$$I = \begin{cases} aB^*T & \text{if } \sum_{\text{day=emergence}}^{\text{current}} T_{\text{day}} < b \\ aB_T \left(1 - \frac{\sum_{\text{day=emergence}}^{\text{current}} (T_{\text{day}} - b)}{\sum_{\text{day=emergence}}^{\text{current}} (T_{\text{day}} - b) + c} \right) & \text{if } \sum_{\text{day=emergence}}^{\text{current}} T_{\text{day}} \geq b \end{cases} \quad (6)$$

where a is a coefficient (ha/kg), b is the critical temperature-sum ($^{\circ}\text{C}$), T is the average temperature for the current day ($^{\circ}\text{C}$) and c is a constant ($^{\circ}\text{C}$).

The performance of the potato crop growth model was tested by comparison of measured (through remote sensing) and simulated leaf area indexes, and by comparison of measured versus simulated final tuber yields.

Fertilizer scenarios

In conventional agriculture in the Netherlands, nitrogen fertilizer additions are high. In areas with factory-farming, organic manure applications are reported to cause leaching of nitrates to the groundwater. Legislation is being implemented to minimize leaching hazards. To evaluate the effects on nitrate leaching of different levels of manure application and of inorganic fertilizer, two scenarios were investigated.

The first scenario was investigated to optimize organic manure additions with respect to ammonia volatilization, nitrate leaching and potato tuber yield levels. The simulation period comprised a period of 17 months, from April 1, 1989 to September 1, 1990. In this period 3 crops were grown: spring barley, followed by a catchcrop (ryegrass) in the same year and by potatoes in the next spring. A surface application of chicken slurry was compared with an

incorporation in the upper 15 cm. The application date was fixed the day after the harvest of the barley crop in August. Both simulations focused on a representative profile for each one of the four soil types present in the field. The best type of application, leading to the smallest loss of N by volatilization and leaching, was thereafter optimized by stepwise adjusting the amount of applied manure until a critical leaching concentration (at 80 cm depth) would not be exceeded over the year following the application. Each optimization step comprised a series of 82 simulations, spatially distributed following a triangular grid with a mesh of 32 m (Fig. 1).

The second scenario evaluated 6 variants of inorganic fertilizer application. The variants were based on the fertilizer advice obtained from:

$$N_{adv} = N_{opt} - aN_{min} \quad (7)$$

where N_{adv} is the advice, N_{opt} is the optimal amount of nitrogen in the rootable zone before planting (evaluated from national trials), a is a crop-dependent factor and N_{min} is the amount of inorganic nitrogen present in the rootable zone before fertilizing. Variants 1 to 5 comprised modifications of the real N_{adv} by factors of 0.25, 0.50, 1.00, 1.50 and 2.00 respectively, and variant 6 modified N_{opt} by a factor of 2 (Table 1).

Nitrate leaching concentrations in the hydrological year between April 1, 1989 and April 1, 1990 were simulated. These loadings were compared with the current (50 mg nitrate/dm³) and with the pursued (25 mg nitrate/dm³) critical concentration levels in leaching water in the Netherlands. Potato dry matter yields were simulated to evaluate the effect of changed fertilizing levels on crop production.

TABLE 1

Description of scenarios analyzed. B and P are regular Dutch fertilizer advice levels for barley and potatoes respectively, where $B = 110 - N$ and $P = 285 - 1.1N$. b, c and p are actual fertilizer gifts for barley, catchcrop and potatoes. N is the amount of mineral nitrogen (kg/ha) in layer 0–60 cm before planting

Scenario	Variant	No. of simulations	Amount given (kg N/ha)		
Chicken slurry	1: surface appl.	4	300		
	2: incorp. 0–15 cm	4	300		
	3: optimization	82	250–500		
Inorganic N	0: initializing run	402	b = B	c = 60	p = P
	1: advice – 75%	402	b = 0.25B	c = 15	p = 0.25P
	2: advice – 50%	402	b = 0.50B	c = 30	p = 0.50P
	3: conform advice	402	b = B	c = 60	p = P
	4: advice + 50%	402	b = 1.50B	c = 90	p = 1.50P
	5: advice + 100%	402	b = 2.00B	c = 120	p = 2.00P
	6: optimal N + 100%	402	b = 220 – N	c = 120	p = 570 – 1.1N

Simulations started with 2 years of fertilizing according to the current advice (variant 0 in Table 1), with initial nitrogen amounts corresponding to the level observed in the field. Thereafter, variants 1 to 6 were simulated, each with an initial nitrogen amount that would be present after two years of standard fertilization. This was done to avoid lagged effects of the current high fertilizer levels on low input scenarios. Next, a period of 17 months was simulated, assuming the same cropping sequence as in the slurry scenarios. All variants were simulated at 402 locations (Fig. 1).

After simulating the effect of varying fertilizer levels, the effect of varying the spatial resolution of application was also investigated. For variants 0 to 3, three methods were compared, different in the way fertilizing advices are obtained, using eq. (7):

- (1) the advice is based on *point-specific* N-status;
- (2) the advice is based on the average N-status for the *soil unit*;
- (3) the advice is based on the *field-average* N-status.

Method (3) follows traditional agricultural practice, method (2) uses available soil survey information and method (1) reflects the maximum attainable spatial precision.

Inputs into the simulation model that varied according to spatial variability observed in the field, were:

- (1) thickness and texture of each functional layer: by location;
- (2) hydraulic characteristics, bulk density and organic matter content: by functional layer;
- (3) depth of groundwater in time: translated from a monitoring series from the same field to other locations by surface topography.

Inputs into the simulation model that were not assumed to vary over the field were:

- (1) initial nitrogen amounts and depth distribution;
- (2) precipitation, air temperature and potential evapotranspiration;
- (3) nitrogen transformation rate constants (though correction for temperature and water content may cause variability in actual rate factors).

Disjunctive kriging

The simulations were aimed at minimizing the risk that nitrate loadings into the groundwater would exceed a critical value of 50 mg nitrate/dm³. It is intuitively clear, that when this risk is to be estimated at locations where no value is known, it will depend on values obtained in the neighbourhood and on the variability. In areas where measured leaching rates are large, there will be a high probability that predicted leaching rates will be large, as well. In areas where leaching is highly variable, uncertainty leads also to a greater estimated risk. This risk can be evaluated by estimating the probability that the 50 mg nitrate/dm³ level is exceeded.

Estimating a probability requires the distribution of the variable "nitrate loading" to be known. Because loadings are concentrations, a skew distribution can be expected, since negative concentrations cannot occur. This may require, that the actual distribution be transformed to a standard normal distribution before probabilities based on the observed data can be calculated. The spatial prediction procedure disjunctive kriging (DK) aims at obtaining an estimator of the conditional probability that a measured variable exceeds a cutoff level at an unvisited location, irrespective of its distribution (Yates et al., 1986; Webster and Oliver, 1989). The probability is conditional, because:

- (i) the spatial correlation structure of the variable is taken into account;
- (ii) the probability is conditioned on a set of observations.

In the application of DK, three assumptions are made:

(i) The original observations $Z(x)$ must be second order stationary; (ii) a function exists that transforms arbitrarily distributed $Z(x)$ to normally distributed $Y(x)$ and that is invertible. This assumption has been proven to be always correct (Kim et al., 1977); (iii) the function produced by the transform ($Y(x)$) has a bivariate normal distribution for each pair of locations.

In DK, a function is sought that is invertible, and that can transform values from whatever distribution to a standard normal distribution. Such a function can be approximated by composing each observation from a number (K) of Hermite polynomials with the appropriate coefficients. The prediction of the variable $Z(x_0)$ on an unvisited point x_0 is thus expanded to a linear combination of predictions in x_0 for each one of K Hermite polynomials:

$$Z_{DK}^*(x_0) = \sum_{k=0}^K C_k H_k^*[Y(x_0)] \quad (8)$$

where the coefficients C_k were obtained from the observations by Hermite integration (Abramowitz and Stegun, 1965); and $H_k[Y(x_0)]$, the value for the k th Hermite polynomial of the normalized variable Y on location x_0 , is estimated by weighing Hermite polynomials from the same order at n neighbouring observation points by:

$$H_k^*[Y(x_0)] = \sum_{i=1}^n b_{ik} H_k[Y(x_i)] \quad (9)$$

where the weights b_{ik} are determined by solving the system:

$$(\rho_{0j})^k = \sum_{i=1}^n b_{ik} (\rho_{ij})^k \quad j=1,2,\dots,n \quad (10)$$

where ρ_{ij} is the autocorrelation between observations i and j .

A predictor of the conditional probability of exceeding a cutoff level is evaluated by defining an indicator function θ :

$$\theta_{y_c} = \begin{cases} 1 & \text{if } Y \geq y_c \\ 0 & \text{if } Y < y_c \end{cases} \quad (11)$$

where y_c is the normalized cutoff level (relating to the actual cutoff level z_c) and Y is the normalized variable (relating to Z). The conditional probability of $Z(x_0)$ exceeding z_c is estimated by the conditional expectation of the indicator function $\theta_{y_c}(Y)$ in location x_0 .

Hereto $\theta_{y_c}(Y(x_0))$ is expanded to a series of Hermite polynomials, so that the conditional probability is estimated by the sum of the predictions of the Hermite polynomials describing $\theta_{y_c}(Y(x_0))$:

$$P^*(x_0) = 1 - G(y_c) + g(y_c) \sum_{k=1}^K H_{k-1}(y_c) H_k^*[Y(x_0)]/k! \quad (12)$$

where H_{k-1} is known; and $H_k^*[Y(x_0)]$ was estimated during the disjunctive prediction procedure; and $G(y_c)$ is the cumulative standard normal probability density for y_c ; and $g(y_c)$ is the standard normal probability density for y_c .

For a detailed description of the DK procedure, reference is made to Yates et al. (1986).

RESULTS AND DISCUSSION

Model performance

A comparison between simulated and measured characteristics is given in Fig. 4a–d. Simulated soil matric potentials agreed well with measurements (R^2 of 0.74) when the soil matrix was unsaturated. Near saturation, simulations deviate from measurements, but differences are small. Simulated inorganic nitrogen contents in the upper meter were simulated reasonably well ($R^2=0.71$), when deviations from measurements (tens of kg N/ha) are compared to fertilizer levels (hundreds of kg N/ha).

Simulated leaf area indexes are generally simulated well ($R^2=0.58$), since most simulated values are found within the 1σ confidence zone associated with the remote sensing estimates (Fig. 4c). Simulated final potato yields are compared to measurements in Fig. 4d. The relatively small R^2 (0.18) is probably caused by variability in the depth distribution of inorganic N at the start of the growing season, which was unknown and therefore assumed homogeneous (Finke, 1992).

Slurry scenarios

Simulation results at four soil profiles, each representative for one soil unit, are given in Table 2. In all soil units, a positive response of crop production

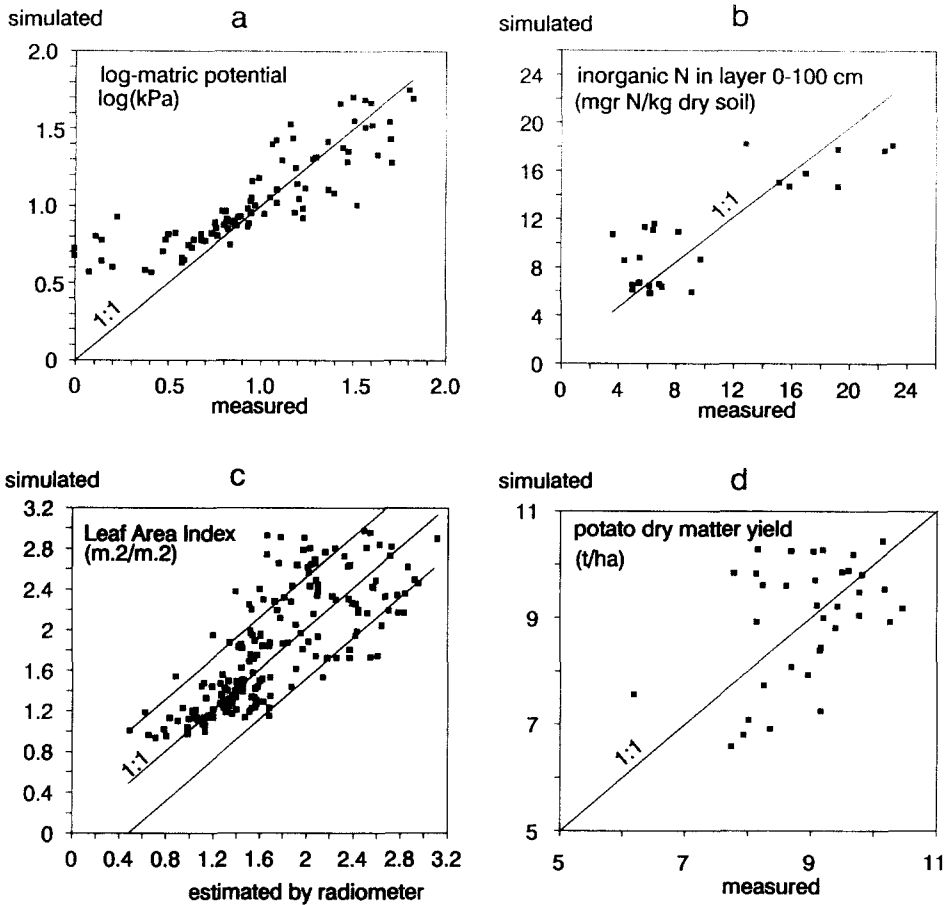


Fig. 4. Simulated and measured characteristics of the water submodel (a), the nitrogen submodel (b) and the potato production submodel for leaf area indexes (c) and final potato yields (d). Two lines parallel to the 1:1 line in (c) indicate one standard deviation confidence zones of the LAI estimated by remote sensing.

TABLE 2

Simulated nitrogen losses (17 months) and dry matter tuber yields in four characteristic soil profiles for surface application (s) and incorporation (i) of 300 kg N/ha slurry. Soil unit codes refer to Fig. 2

Soil unit	NH ₃ -volat. (kg N/ha)		NO ₃ -leaching (kg N/ha)		Plant uptake (kg N/ha)		Yield (t/ha)	
	s	i	s	i	s	i	s	i
A	193.3	151.6	9.1	10.3	697.7	701.2	11.3	12.0
B1	193.6	151.9	6.7	7.4	657.2	679.4	10.4	12.0
B2	192.6	150.9	6.9	8.0	646.1	664.4	8.7	9.5
C	194.0	152.5	7.3	8.0	672.5	696.4	10.8	12.3

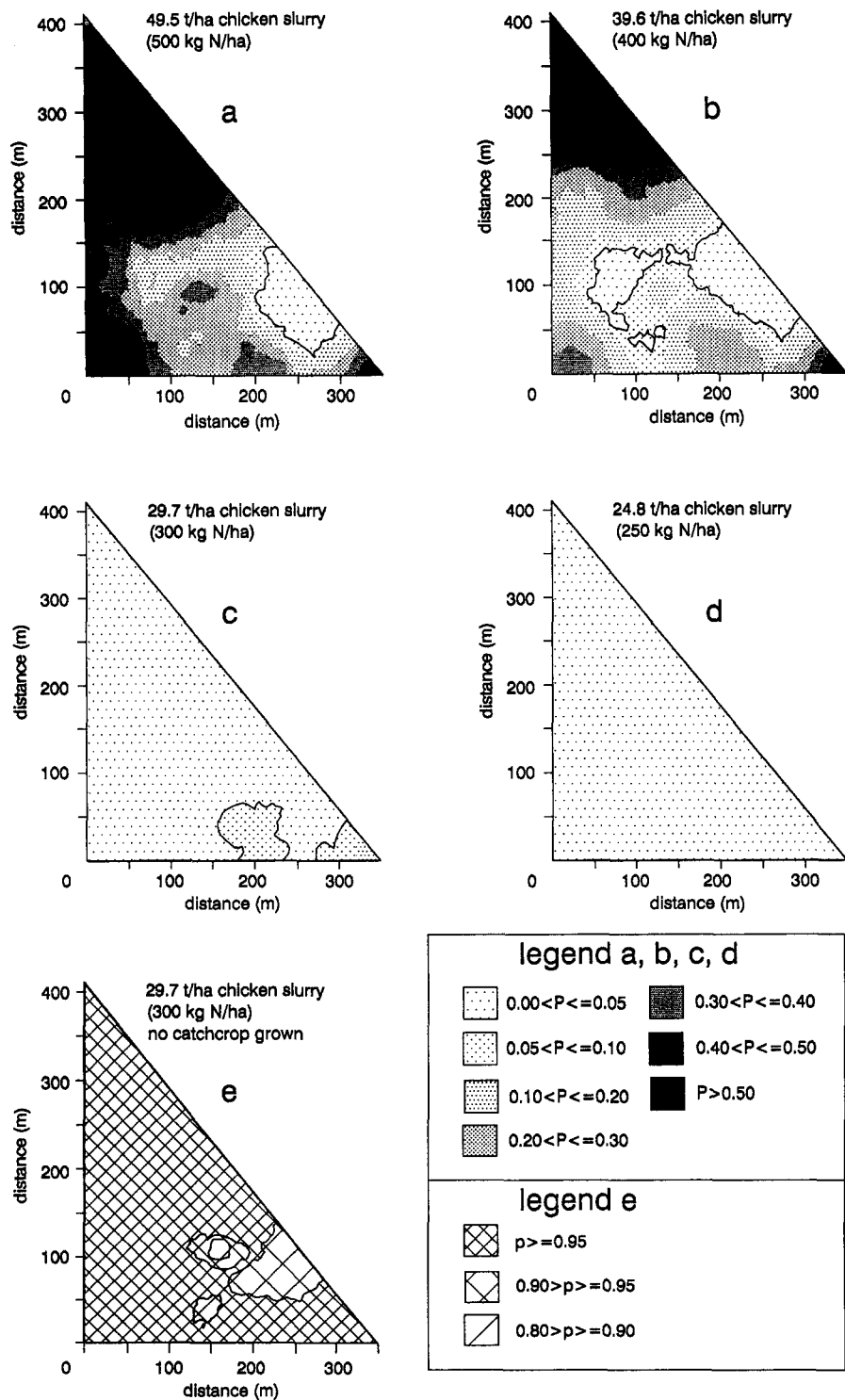


Fig. 5. Maps of the probability (P) that leaching exceeds $50 \text{ mg NO}_3\text{-N/dm}^3$ at slurry applications from 500–250 kg N/ha when a catchcrop is grown (a to d) or not grown (e).

TABLE 3

Comparison of field specific and soil specific maximum amounts of slurry not leading to exceedance of the leaching criterium. Soil codes refer to Fig. 2

Soil unit	Area (%)	Application of slurry			
		soil specific		field specific	
		level (t slurry/ha)	yield (t dm/ha)	level (t slurry/ha)	yield (t dm/ha)
A	23	29.7	9.4	24.8	9.1
B1	19	39.6	9.5	24.8	8.4
B2	8	39.6	7.3	24.8	6.3
C	50	24.8	9.2	24.8	9.2
Field		tonnage	tonnage	tonnage	tonnage
		215.1	65.7	177.9	63.1

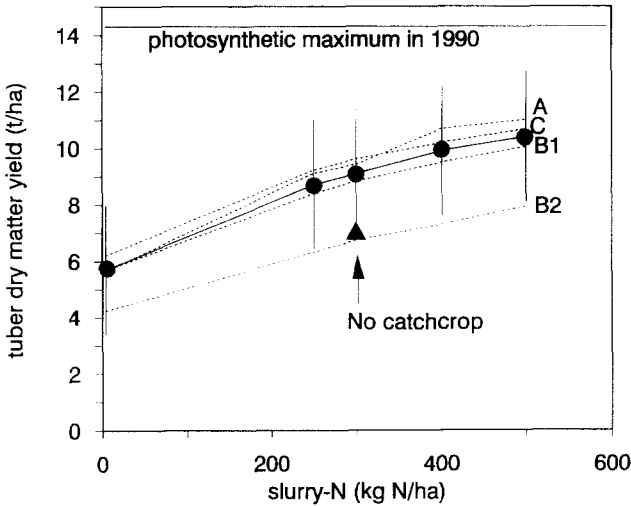


Fig. 6. Simulated average and soil specific crop response in 1990 to slurry additions in 1989. A, B1, B2 and C refer to soil units (see Fig. 2); solid lines connects average crop response and zones of 1 standard deviation, dashed lines connect soil-specific responses; dots represent average yields; triangle represents average yield for scenario without a catchcrop.

and plant nitrogen uptake occurred when slurry was incorporated into the upper 15 cm in the soil. In case of surface application, nitrate leaching was slightly lower, but this was more than compensated for by the far higher ammonia volatilization. Both crop production and total nitrogen losses to the environment were more favourable in case of incorporation. For these reasons, further scenario analyses considered slurry applications to be incorporated into the soil.

Simulated effects on nitrate leaching of slurry additions of 500, 400, 300 and 250 kg N/ha are presented as leaching probability maps in Fig. 5. The criterion that "nowhere in the field the probability of exceeding the cutoff-leaching concentration may be greater than 5%" was met with a slurry addition equalling 250 kg N/ha. The important role of the catchcrop in minimizing nitrate leaching concentrations is obvious from the leaching probability map at 300 kg N/ha slurry addition when no catchcrop is grown (Fig. 5e). Comparing leaching probability maps with the soil map, shows that soil units A and C (Fig. 2) are more sensitive to nitrate leaching than soil units B1 and B2. This result was used to determine soil specific slurry application rates. If the slurry gift would be 300 kg N/ha for soil A, 400 kg N/ha for soils B1 and B2, and 250 for soil C, the leaching criterion would still be met, but 21% more slurry could be applied to the whole field, and the crop yield for the whole field would increase by 4% (Table 3).

Simulated potato yield response to the various slurry gifts and its spatial variation is presented in Fig. 6. Slurry additions higher than 250 kg N/ha still showed a positive effect on potato yields, but the differences are not large. The photosynthetic maximum was not reached by far, indicating that something else than nitrogen deficiency depressed crop yields. This cause has been identified as moisture stress (Finke, 1992), and explained why the variability in crop yields (Fig. 6) was not decreasing when slurry-N additions increased. Different soil units showed a different response to slurry-N (Fig. 6). When no catchcrop would be grown, not only would leaching drastically increase, but also crop yields would be significantly less (Fig. 6).

Inorganic nitrogen fertilizer scenarios

Simulated nitrate leaching concentrations did not exceed the criterion based on the current threshold concentration of 50 mg nitrate-N/dm³. However, the pursued threshold concentration of 25 mg nitrate-N/dm³ was exceeded in case of scenario variants 0 and 6 (Table 4).

Variants 0 and 3 were identical in terms of the way the fertilizer level was calculated (see Table 1). The strong difference in probability of leaching between variants 0 and 3 must therefore be attributed to a lagged effect of high fertilizer levels in the past, which created a pool of (organically bound) nitrogen that was emptied largely during the simulation period of variant 0. The high input scenario variant 6 resulted in exceedance of the threshold probability of 5% in part of the field, which indicates that this scenario will not reduce leaching to the pursued level. Scenario variants 1 to 5 would not violate the threshold probability during the simulation period.

In Fig. 7, the average and soil-specific response of potato yield to the fertilizing scenario is presented. Scenario variant 0 resulted in clearly higher average yields than variant 3, because more inorganic nitrogen is mineralized dur-

TABLE 4

Percentage of the area not satisfying quality criteria based on the probability that a leaching concentration greater than 25 mg nitrate-N/dm³ is exceeded. Variants refer to Table 1

Variant	Probability greater than				
	0.50	0.25	0.10	0.05	0.025
0	66.8	94.1	99.0	99.5	99.8
1	0	0	0	0	0
2	0	0	0	0	0
3	0	0	0	0	0
4	0	0	0	0	0
5	0	0	0	0	0
6	0	0	0	1.4	15.5

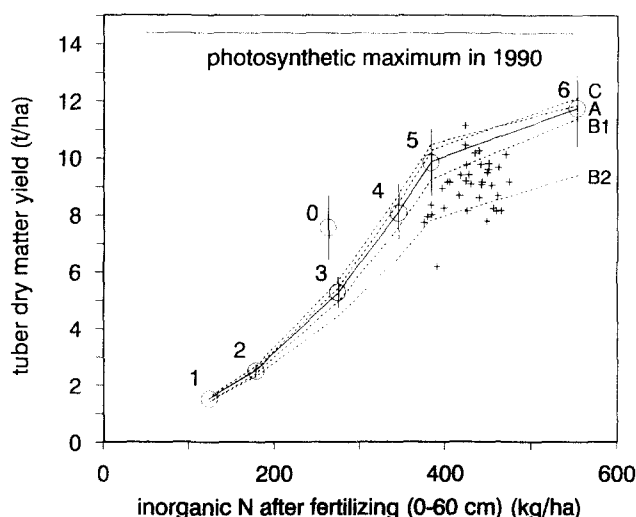


Fig. 7. Simulated average and soil-specific crop response to fertilizer levels in 1990. A, B1, B2 and C refer to soil units (see Fig. 2); 0 to 6 refer to fertilizer scenarios (see Table 1); solid line connects average crop-response and zones of 1 standard deviation, dashed lines connect soil-specific responses; plusses represent field measurements in 1990.

ing the growing season. The vertical bars in Fig. 7 indicate that crop yield becomes more variable when fertilizer gifts are higher. This must be attributed to the increasing importance of water-availability as a factor that is stressing crop growth. Soil units B2 and, to a lesser extent, B1 show a clearly weaker response to N availability, because capillary rise in these soils is limited by a thick clay loam layer, causing the actual transpiration to be lower than the potential transpiration.

In case of scenario variant 6, the pursued leaching concentration of 25 mg/dm³ was exceeded only in soil unit C. Soil unit specific fertilizing according

TABLE 5

Variability (coefficients of variation) of simulated yields, nitrate leaching concentrations and residual inorganic nitrogen after 17 months for plot-specific, soil-specific and field-specific fertilizing. Variants refer to Table 1

Variant	Variable	Spatial resolution of application		
		plot CV (%)	soil CV (%)	field CV (%)
0	yield	14.97	14.84	14.80
1		6.41	6.43	6.47
2		7.58	7.55	7.62
3		10.28	9.87	9.88
0	leaching conc.	20.65	20.65	20.65
1		68.90	68.90	68.90
2		59.61	59.61	59.61
3		38.63	38.63	38.63
0	residual N	6.36	6.47	6.49
1		3.58	3.63	3.63
2		3.95	4.02	4.02
3		5.37	5.50	5.51

to scenario variant 5 for soil C and according to variant 6 for units A, B1 and B2 would satisfy the leaching criterion. This would result in a field yield of 77.0 ton dry matter whereas field-specific fertilizing according to scenario variant 5 would produce 70.7 ton dry matter. Soil specific fertilizing would thus increase field yields by 9%.

A comparison of some simulation results of point-specific, soil unit specific and field-specific fertilizing for variants 0 to 3 (Table 1) is made in Table 5.

Differences between treatments are small or absent. The variability of yields would decrease when fertilization would change from field-specific to soil-specific only when fertilizer levels are low (variants 1 and 2). Further differences between soil- and field-specific fertilizing are negligible. The residual amount of inorganic nitrogen after 17 months is consequently more variable for field-specific fertilizer applications than for point-specific applications. This indicates that, on the long run, plot-specific fertilizing may produce a less variable nitrogen status than field-specific fertilizing.

As a result, it is concluded that fertilizing by soil instead of fertilizing by field would not have a significant effect on crop yields when it pursues a homogeneous nitrogen distribution over the field. When fertilizer levels are obtained from soil specific response characteristics (Fig. 7), soil specific fertilizing may result in raising average yields.

CONCLUSIONS

(1) Scenario analyses by simulation modelling form an operational tool to evaluate the effect of fertilizer management. When simulation model param-

eters reflect soil spatial variability, variability of simulation results can be used to map the probability that critical levels are exceeded. A promising tool to determine these probabilities is the method of disjunctive kriging.

(2) Both leaching response and crop yield response to the slurry application level differ by soil unit. Soil specific optimal slurry treatments (optimal in the sense that leaching criterion is not exceeded) results in higher total applications and higher yields than field specific optimal treatments.

(3) Soil specific nitrogen fertilizer advices did not result in different leaching or crop yields when compared to field- or point-specific advices. Soil specific crop response curves show that the response to inorganic nitrogen differs by soil type.

(4) Spatial variability of yields increased when nitrogen levels increased. This is caused by an increasing variability of the transpiration deficit due to differences in foliar growth as governed by water availability.

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